

The Effect of Sequence Distribution on Glass Transition in the Theory of the Cooperative Behaviour of Random Copolymers

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Summary

The description of the cooperative behaviour of polymers in the glass transition region according to ADAM and GIBBS (1965) has been extended to comprise the dependence of glass transition temperature, T_g , on the chemical composition of random copolymers if the distribution of dyads of comonomer units is included. The compositional dependence of T_g is expressed in terms of (i) differences between the isobaric heat capacities in the liquid and glassy states, and of (ii) the equilibrium T_g temperatures of the parent homopolymers and of the alternating copolymer. Validity of this theory was verified by comparison with data on styrene/methyl methacrylate and styrene/n-octyl methacrylate copolymers; the results indicate that the relations derived agree quantitatively with the experiment similarly to the equations suggested earlier by JOHNSTON (1976) and BARTON (1970). Moreover, these relations are based on a physically better justified approach to the glass transition phenomenon.

Introduction

The shape of the compositional dependence of the copolymer glass transition temperature, T_g , cannot in many cases be predicted only from the T_g 's of both parent homopolymers. The curvatures or even the extremes sometimes observed in the dependences of T_g of random copolymers on their overall chemical composition have been explained by the effect of sequence distribution (BARTON 1970, JOHNSTON 1976). In the dyad approximation, equations can be constructed for these dependences containing the T_g 's of both parent homopolymers and of the alternating copolymer. (Similarly, equations can be constructed in the triad or higher approximation, which, unfortunately, contain experimentally inaccessible parameters.)

Several relations have been suggested for the

description of the sequence distribution effect. By extending FOX's equation (1956), JOHNSTON (1976) arrived at a relation in which the reciprocal copolymer T_g equals the sum of the reciprocal T_g 's of both parent homopolymers and of the alternating copolymer, all the three contributions being weighted by the weight fractions of the respective dyads. The BARTON's approximation (1970) is based on the Gibbs-DiMarzio theory (DiMARZIO and GIBBS 1959) and holds, strictly speaking, only for the equilibrium transition temperature, T_2 , as introduced in their theory; here, the copolymer T_2 (or T_g) is assumed to equal the sum of the T_2 's (or T_g 's) of both parent homopolymers and of the alternating copolymer, all the three terms being weighted by the mole fractions of rotatable bonds pertaining to the respective dyads. Although both approaches are phenomenological, Johnston's equation can be regarded rather as an isochoric one, while Barton's equation is isentropic with respect to T_g . UEMATSU and HONDA (1965, 1966) suggested another isentropic approach, using contributions of stiffness energy. Barton, and Uematsu and Honda consider the configurational entropy at T_g to vanish. Although the equations thus obtained adequately describe some experimental dependences, it has been shown that the glass transition is neither an isochoric nor an isentropic phenomenon (HAVLÍČEK et al. 1980 b).

All experimental procedures used in the determination of T_g examine the glass transition in the range of approximately the same relaxation times. Hence, a comparison between the theory and experimental data is feasible by regarding the glass transition as an isochronic phenomenon. In a preceding paper (HAVLÍČEK et al. 1980 a), the theory of the cooperative behaviour of polymers (ADAM and GIBBS, 1965) was employed to describe the compositional dependence of the random copolymer glass transition temperature without taking into account the effect of sequence distribution. In this paper, the effect of sequence distribution in the dyad approximation is involved.

Theory

A model of the cooperative rearrangement of polymer molecules and their parts was suggested by ADAM and GIBBS (1965). For the probability of a cooperative configurational change, they derived the relation

$$W(T) = A \exp[-m/TS_c(T)] \quad (1)$$

in which S_c is the configurational entropy, m is a

quantity related to the topological and energetical features of the cooperative transition, and A is a frequency factor (its temperature and compositional dependence need not be taken into account). The configurational entropy may be approximated by

$$S_c(T) = \Delta C_p \ln(T/T_2) \quad (2)$$

where ΔC_p is a difference between the isobaric heat capacities below and above the glass transition. At a hypothetical T_2 temperature which lies approx. 50 K below T_g , the number of configurations attainable by the material drops to unities, whence the configurational entropy $S_c = 0$.

If the constant relaxation time of the configurational change τ ($\tau \sim 1/W$) is taken as the criterion of the glass transition, we can write:

$$\begin{aligned} W^c(T_g^c) &= W^{AA}(T_g^{AA}) = W^{BB}(T_g^{BB}) = W^{AB}(T_g^{AB}) = \\ &= W^{ij}(T_g^{ij}) \end{aligned} \quad (3)$$

Here, as well as in the following equations, the quantities with the superscripts c , AA , BB and AB relate to any random copolymer, the parent homopolymers A and B , and the alternating copolymer, respectively.

For the quantities m and ΔC_p , molar additivity in the dyad approximation is assumed:

$$m^c = \sum_{ij} x^{ij} m^{ij} \quad (4)$$

$$\Delta C_p^c = \sum_{ij} x^{ij} \Delta C_p^{ij} \quad (5)$$

In the Eqs (4) and (5), and also in the following ones, summations are performed for $ij = AA, BB, \text{ and } AB$; x^{ij} are mole fractions of the respective dyads. Since T_2^c is the temperature of zero configurational entropy, it obeys Barton's equation (BARTON 1970), which is additive in mole fractions of rotatable bonds y^{ij} corresponding to the dyad ij , i.e.

$$T_2^c = \sum_{ij} y^{ij} T_2^{ij} \quad (6)$$

here, $y^{ij} = x^{ij}(n^i + n^j)/2(x^n^{AA} + x^n^{BB})$, where n^A and n^B respectively are the numbers of rotatable bonds in the monomeric units A and B ; x^A and x^B are mole fractions of these units. By combining equations (1) - (6),

we obtain for the glass transition temperature of a random copolymer in the dyad approximation

$$T_g^c \Delta C_p^c \ln(T_g^c/T_2^c) = \sum_{ij} x^{ij} T_g^{ij} \Delta C_p^{ij} \ln(T_g^{ij}/T_2^{ij}) \quad (7)$$

If we assume the molar additivity of configurational entropy at $T = T_g$, viz.

$$S_c^c(T_g^c) = \sum_{ij} x^{ij} S_c^{ij}(T_g^{ij}) \quad (8)$$

instead of the isochronic criterion discussed above, we obtain a similar relation for the copolymer glass transition:

$$\Delta C_p^c \ln(T_g^c/T_2^c) = \sum_{ij} x^{ij} \Delta C_p^{ij} \ln(T_g^{ij}/T_2^{ij}) \quad (9)$$

Comparison with Experiment and Discussion

Two copolymer systems were chosen in order to verify the theory, namely, styrene/methyl methacrylate (S/MMA) and styrene/n-octyl methacrylate (S/OMA). The ΔC_p values were determined for all samples by the DSC method. The samples were first cooled at a rate of 10 K/min and then heated at the same rate. Heating run was used in the evaluation. Syntheses of copolymers, experimental procedure and evaluation of T_g 's are given elsewhere (PODEŠVA and BIROŠ 1980). The data support the suitability of Eq.(5) as shown in Fig.1. Extrapolation based on Eq.(5) was used for the determination of the experimentally inaccessible ΔC_p value for POMA. Mole fractions of dyads were calculated from the relations (HARWOOD and RITCHEY 1964)

$$x^{AB} = 4x^A x^B / \left\{ 1 + [1 + 4x^A x^B (r^A r^B - 1)]^{1/2} \right\} \quad (10)$$

where r^A and r^B are monomer reactivity ratios, and

$$x^{AA} = x^A - x^{AB}/2 \quad (11)$$

Input data used in equations (7) and (9) are given in Table I.

TABLE I

Input data for the calculation of the compositional dependences of the random copolymer glass transition temperatures

polymer	T_g^b , K	T_2 , K	ΔC_p , J/mol K	n^g)
PS	373	324.5 ^{c)}	32.5	3
PMMA	390	305.1 ^{c)}	20.1	4
S/MMA ^{a)}	371	321 ^{d)}	28.0	-
POMA	245	195 ^{d)}	20 ^{f)}	11
S/OMA ^{a)}	270	250 ^{e)}	30.1	-

a) alternating copolymer; b) PODEŠVA and BIROŠ 1980; c) HAVLÍČEK et al. 1978; d) $T_2 = T_g - 50$ K; e) adjusted for a better fit between Eq. (7) and experimental data; f) adjusted using Eq. (5); g) number of rotatable bonds.

Since neither homopolymers nor alternating copolymers were studied by viscoelastic methods, the T_2 values for PS and PMMA were taken from a paper by HAVLÍČEK et al. (1978). For the alternating S/MMA and S/OMA copolymers and for poly(n-octyl methacrylate) (POMA), it was assumed that $T_2 = T_g - 50$ K, where for T_g of POMA the extrapolated value 245 K was employed (PODEŠVA and BIROŠ 1980). It appeared that if we used somewhat higher values of T_2 for the alternating S/OMA copolymer, a better agreement was achieved between experiment and theory; for this reason, $T_2 = T_g - 20$ K was adjusted for this copolymer.

Compositional dependences of the glass transition temperatures of both random copolymer systems are compared in Fig. 2. It can be seen that the fit of experimental points with the curves predicted by Eq. (7) is satisfactory. This holds mainly for the S/MMA system, for which in Eq. (7) reliable input parameters were available (with the exception of T_2 of the alternating copolymer). For this system, the fit with Eq. (7) is better than with Johnston's and Barton's equations: the arithmetic mean from absolute deviations of experimental copolymer T_g 's from theory, d , equals 0.9, 1.5, and 2.3 K, respectively. A poorer fit is observed for the S/OMA system: for Eq. (7), Johnston's and Barton's equations, $d = 5.6, 2.7,$ and 5.3 K, respectively. Though the physical quantities ΔC_p and T_2 which appear in Eqs (7) and (9) may be subjected to a considerable error, numerical calculation shows that these errors are not substantially reflected in the compositional

dependence of T_g : e.g., with the S/MMA system changes in ΔC_p by 10% or in T_2 by 10 K lead to changes in T_g^C in the range ± 1 K.

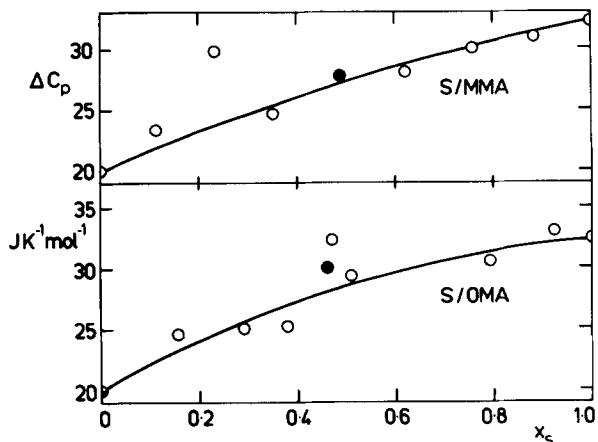


Figure 1. Dependence of a difference between the isobaric heat capacities below and above glass transition, ΔC_p , of random styrene/methyl methacrylate (S/MMA) and styrene/n-octylmethacrylate (S/OMA) copolymers on the mole fraction of styrene, x_s . Solid lines correspond to Eq.(5); \circ - homopolymers and random copolymers; \bullet - alternating copolymers; \ominus - extrapolated value

The results suggest that, with the systems under study, Eq.(7) may be considered equally adequate in a quantitative description of the dependences of T_g of random copolymers on their overall chemical composition as equations of Johnston and Barton, analyzed in detail earlier (PODEŠVA and PROCHÁZKA 1979, PODEŠVA and BIROŠ 1980). The contribution made by Eq.(7) consists predominantly in a physically better justified approach to the glass transition phenomenon.

We also found the differences between the results yielded by Eqs(7) and (9) to be smaller than the experimental error of the determination of T_g (5 K at most, in the part of the compositional scale where T_g

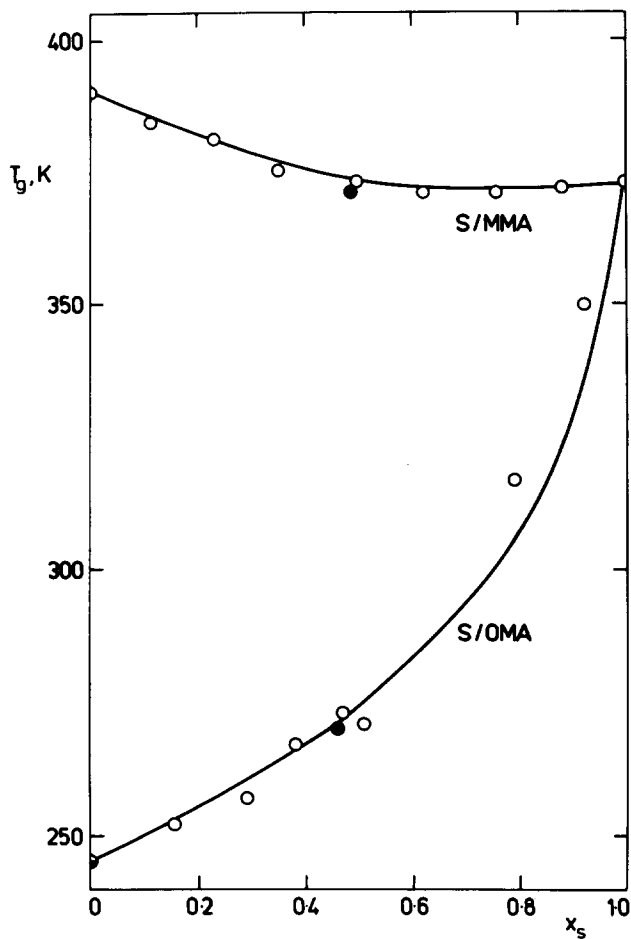


Figure 2. Dependence of the glass transition temperature, T_g , of random styrene/methyl methacrylate (S/MMA) and styrene/n-octyl methacrylate copolymer on the mole fraction of styrene, x_s . Solid lines correspond to Eq.(7); \circ - homopolymers and random copolymers; \bullet - alternating copolymers; \ominus - extrapolated value (PODEŠVA and BIROŠ 1980)

changes steeply, otherwise 1-2 K). This fit suggests that, respecting the model of Adam and Gibbs, the conservation of the value of relaxation time at T_g is adequately described by the additivity of the configurational entropy of random copolymers on the dyad approximation.

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